

# Interaction Between Graphene-Coated SiC Single Crystal and Liquid Copper

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The wettability of graphene-coated SiC single crystal ( $C_{Gn}/SiC^{sc}$ ) by liquid Cu (99.99%) was investigated by a sessile drop method in vacuum conditions at temperature of 1100 °C. The graphene layer was produced via a chemical vapor deposition routine using 4H-SiC single crystal cut out from 6" wafer. A dispensed drop technique combined with a non-contact heating of a couple of materials was applied. The Cu drop was squeezed from a graphite capillary and deposited on the substrate directly in a vacuum chamber. The first Cu drop did not wet the  $C_{Gn}/SiC^{sc}$  substrate and showed a lack of adhesion to the substrate: the falling Cu drop only touched the substrate forming a contact angle of  $\theta_0 = 121^\circ$  and then immediately rolled like a ball along the substrate surface. After settling near the edge of the substrate in about 0.15 s, the Cu drop formed an asymmetric shape with the right and left contact angles of different values ( $\theta_R = 86^\circ$  and  $\theta_L = 70^\circ$ , respectively), while in the next 30 min,  $\theta_R$  and  $\theta_L$  achieved the same final value of  $\sim 52^\circ$ . The second Cu drop was put down on the displacement path of the first drop, and immediately after the deposition, it also did not wet the substrate ( $\theta = 123^{\circ}$ ). This drop kept symmetry and the primary position, but its wetting behavior was unusual: both  $\theta_R$  and  $\theta_L$  decreased in 17 min to the value of 23° and next, they increased to a final value of 65°. Visual observations revealed a presence of  $\sim$  2.5-mm-thick interfacial phase layer reactively formed under the second drop. Scanning electron microscopy (SEM) investigations revealed the presence of carbon-enriched precipitates on the top surface of the first Cu drop. These precipitates were identified by the Raman spectroscopy as double-layer graphene. The Raman spectrum taken from the substrate far from the drop revealed the presence of graphene, while that obtained from the first drop displacement path exhibited a decreased intensity of 2D peak. The results of SEM investigations and Raman spectroscopy studies suggest that the presence of graphene layer on the SiC substrate suppresses but does not completely prevent chemical interaction between liquid Cu drop and SiC. Both chemical degradation (etching) and mechanical degradation of the graphene layer during drop rolling due to high adhesion of the Cu drop to the SiC substrate are responsible for mass transfer through the 2nd drop/substrate interface that in turn results in significant changes of structure and chemistry of the drop and the interface.

Keywords graphene, liquid Cu, Raman spectroscopy, reactivity, sessile drop, wettability

## 1. Introduction

In recent years, the outstanding properties of carbon nanotubes and graphene have inspired the researchers with the idea of its possible use in metal matrix composites (MMCs) as a constituent significantly improving thermal properties (thermal conductivity and thermal expansion) of these materials, particularly important for thermal management applications

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M. Homa, J.J. Sobczak, A. Kudyba, G. Bruzda, and R. Nowak, Foundry Research Institute, 73 Zakopianska Str., 30-418 Krakow, Poland; N. Sobczak, Foundry Research Institute, 73 Zakopianska Str., 30-418 Krakow, Poland; and Institute of Precision Mechanics, 3 Duchnicka Str., 01-796 Warsaw, Poland; and K. Pietrzak and M. Chmielewski, Institute of Electronic Materials Technology, 133 Wolczynska Str., 01-919 Warsaw, Poland; and W. Strupiński, Politechnika Warszawska Wydział Fizyki, 75 Koszykowa Str., 00-662 Warsaw, Poland. Contact e-mail: marta.homa@iod.krakow.pl. in electronic and automotive industry, aerospace, fuel cells, etc. (Ref 1-6). While some enhancement of thermal properties of MMCs with carbon nanotubes seem to be attainable (Ref 7), a large-scale manufacturing of graphene reinforced MMCs is accompanied by still difficult-to-overcome problems, mainly related with the occurrence of the agglomeration of graphene phase due to electrostatic forces (Ref 8) and a weak interfacial bonding between the graphene flakes and metal matrix (Ref 9). A microelectronic packaging is another possible graphene application field, e.g., as transparent conducting layers or fillers in solder alloys that could reduce the cost or energy consumption and improve the reliability of electronic components (Ref 10-13). For all above-mentioned graphene-based solutions, information on interaction between liquid metals and graphenecoated materials, particularly wetting behavior and interfaces, is of a great practical importance for different liquid-assisted processes.

To our best knowledge, reported literature data on wetting properties of graphene-coated surfaces are limited to water and organic liquids showing the wetting behavior and the contact angle values similar to those of uncoated surfaces (Ref 14-18). This phenomenon, described by Rafiee et al. (Ref 19) as the graphene wetting transparency, has been also theoretically predicted by molecular dynamic simulations (Ref 19) and confirmed experimentally for different low-temperature liquids and various types of substrate materials [Cu foil (Ref 16), HOPG (Ref 17), graphite (Ref 17), Si (Ref 19)]. However, there is no available report on wetting behavior of high-temperature liquids on graphene-coated materials. The first attempt to investigate wetting properties of a liquid metal on graphene has been done by Sobczak et al. (Ref 20) by using liquid tin and graphene-coated Cu substrate (CGn/Cu). It was demonstrated that the presence of graphene layer on the Cu substrate delays the wetting process, as compared to the uncoated Cu substrate, while wetting behavior of liquid tin on the CGn/Cu substrate was found to be very similar to that on uncoated pure Cu. Thus, the results obtained in Ref 20 did not clearly confirm the existence of graphene wetting transparency effect with liquid tin as it was previously reported for inorganic liquids or water in Ref 14-19. On the other hand, the results of structural characterization performed by Sobczak et al. (Ref 20) on crosssectioned solidified sessile drop couples showed the presence of interfacial intermetallic compound layer. It was proposed that this layer can be formed due to the mass transfer between the Cu substrate and liquid Sn, i.e., under conditions when the graphene layer does not play a role of a barrier for Sn atoms. The above contradictions were explained by the possible reconstruction of graphene layer during a high-temperature interaction with liquid tin leading to the formation of structural discontinuities through which liquid tin reacts with the substrate and, consequently, the graphene wetting transparency effect is masked or hindered (Ref 20).

This paper reports the results of in situ observation of hightemperature behavior of molten Cu drops in contact with graphene layer deposited on SiC single-crystalline substrate using the same testing procedure and experimental facility as those previously used for the  $Sn/C_{Gn}/Cu$  system in Ref 20.

## 2. Experimental

#### 2.1 Materials

The materials used were Cu of 99.99% purity (Hutmen S.A. Company, Poland) and graphene-coated silicon carbide singlecrystalline substrate ( $C_{Gn}/SiC^{sc}$ ) produced by the Institute of Electronic Materials Technology (Warsaw, Poland). The graphene layer was produced by chemical vapor deposition (CVD) process on conductive SiC substrates described in detail earlier (Ref 21). The produced  $C_{Gn}/SiC^{sc}$  sample was kept in sealed capsules in order to eliminate the risk of contamination.

#### 2.2 Methods

The sessile drop (SD) method (Ref 22, 23) was applied to investigate a high-temperature wetting behavior of molten Cu on  $C_{Gn}/SiC^{sc}$  substrate using an experimental complex described in details in Ref 23. Directly before loading into vacuum chamber, the graphene-coated SiC substrate was taken from a sealed capsule and placed on alumina support located inside tantalum-resistant heater of vacuum chamber. In order to avoid the effects of native oxide film on metal sample as well as to eliminate the impact of heating history on wetting behavior, the research was performed under ultrahigh vacuum (UHV) conditions using a non-contact heating of a metal and a substrate combined with capillary purification (cp) as described in the works (Ref 22, 23). For this purpose, also directly before loading into vacuum chamber, the Cu sample was cleaned mechanically and ultrasonically in isopropanol and placed inside a ceramic capillary (made of either graphite or alumina) positioned above the  $C_{Gn}/SiC^{sc}$  substrate. After evacuation of gases and achieving the vacuum of about  $p = 2 \times 10^{-5}$  mbar by means of a turbomolecular pump, the setup was heated to the test temperature of 1100 °C with a rate of 10 °C/min and then the Cu drops were deposited on the substrate.

During the whole course of wettability experiments, the types and amounts of residual gases in the vacuum chamber were monitored in real-time using Pfeiffer Prisma QMS200 quadrupole device, while the images of the drop/substrate couple were recorded by MC1310 high-speed high-resolution camera with a rate of 50 frames per second. The collected images were used to estimate the contact angle values by ASTRA2 software [IENI-CNR, Italy (Ref 24, 25)]. The software allows determining the contact angle on left and on right sides of a drop by an automatic image analysis with systematic uncertainty less than  $\pm 2^{\circ}$ . The collected images were also used for making movies of the test performed at high temperature (see SUPPLEMENTARY 1-3). After each wettability test, the system was cooled with a rate of about 20 °C/min.

The structural characterization was performed on both the starting materials and the solidified sessile drop  $Cu/C_{Gn}/SiC$  couples using the following techniques:

- (1) Scanning probe microscopy (SPM) combined with Raman spectroscopy using NTEGRA Spectra system (NT-MDT Europe). The Raman spectra were taken under ambient conditions using an diode pumped solid-state laser with a wavelength of 473 nm. The incident laser power was 50 mW, the spot size  $\sim 1 \ \mu m$  in diameter and the exposure time 30 s.
- (2) Scanning electron microscopy (SEM) using TM3000 Hitachi device equipped with energy-dispersive x-ray spectroscopy (EDS) analyzer.

### 3. Results and Discussion

The results of SPM analysis of the CGn/SiC substrate showed a characteristic terraced structure on the surface of single SiC crystal (that was recognized as the effect of polishing) (Fig. 1a). The obtained representative Raman spectrum of graphene produced on SiC (001) was characterized by the presence of peaks related to SiC (1300-1750  $\text{cm}^{-1}$ ) and three major bands of graphene, namely D, G and 2D (Fig. 1b). Their Raman shifts for a laser wavelength of 473 nm are 1414, 1603 and 2753  $\text{cm}^{-1}$ , respectively. A full width at half maximum (FWHM) of 2D peak with a value of about 58 cm<sup>-1</sup> indicates that the tested graphene is a two-layer product (Ref 26). The lower intensity of D peak as compared to peaks G and 2D proves that graphene is only mildly defective. The measurement repeated several times in different places on the substrate, both on the surface and on the edges of SiC terraces, showed a spectrum typical of graphene, which confirms the continuity of mildly defective layer of  $C_{Gn}$ .

#### 3.1 Wettability Tests with Alumina Capillary

The first wettability test was performed with an alumina capillary using a continuous contact of the Cu drop with the



**Fig. 1** A surface characterization of graphene layer obtained on SiC single crystal: (a) SPM image of the graphene on 4H-SiC (0001) substrate; (b) a Raman spectrum

capillary during drop deposition on the substrate (SUPPLE-MENT #1), i.e., after squeezing the Cu drop, the capillary was moved down to establish a contact between the drop and the substrate. Subsequently, the capillary was moved up in order to detach it from the drop. However, rising the capillary was accompanied with lifting the whole drop/substrate couple because the drop was well bonded to the substrate. A similar behavior and problems with the Cu drop detachment from the capillary were observed with uncoated SiC single-crystal substrate. On the contrary, when the same test was performed with graphite substrate, the Cu drop did not establish a good bonding with graphite since every rise in the capillary after the drop deposition caused a complete detachment of the drop from the substrate and no residual metal was observed on the substrate surface. The effect of the substrate material on dissimilar behavior of the Cu drop during rising of the capillary, when the drop is connected with both the capillary and the substrate, is in a good agreement with existing knowledge. The Cu/C system is recognized as non-wetting and non-reactive; thus, adhesion between Cu and all carbon materials is week, independently on carbon allotropic form (Ref 27). On the contrary, a strong interaction between Cu and SiC (Ref 28-33) was reported, hence substantial adhesion between the Cu drop and the SiC substrate is obvious. The above observations demonstrate the similarity of the Cu drop behavior with graphene-coated and graphene-free SiC substrates, thus suggesting that under conditions of this study, the graphene layer is transparent for liquid Cu.

In the same test after the first attempt, the second lowering and re-raising the capillary resulted in a successful drop detachment but also in the appearance and floating of large solid-like fragment on the drop surface (Fig. 2). During holding at the test temperature, this fragment was moved to the top of the drop and settled in a tilled position on the capillary resulting in the deformation of initially symmetrical drop. This in turn made difficult reliable measurements of the contact angles formed between the Cu drop and the substrate (t = 0 min,  $\theta_{av} = 112^\circ$ ; t = 30 min,  $\theta_{av} = 82.6^\circ$ ).

After deposition on substrate, the Cu drop formed average value contact angle of  $\theta_{av} = 112^{\circ}$  ( $\theta < 90^{\circ}$ ). Contact angle was not stable with time and started decreasing to form the final value of  $\theta_{av} = 82.6^{\circ}$  after 30 min.

The SEM top view observations of the solidified drop (Fig. 3a and b) revealed a large round pancake-like fragment dark gray in color. Figure 3(c) shows a higher magnification of rectangle marked in Fig. 3(b) with EDS analysis of chemical composition in three well-distinguished regions (in at.%): 1-dark region enriched in carbon and containing only 1.4% Si; 2-bright region rich in Cu and containing 5.7% Si; 3-dark region, also enriched in carbon, corresponding to the drop-side surface of wrapped "pancake" fragment. More detailed EDS analysis of the wrapped region (Fig. 3d) displays mainly carbon (94.7% in its dark-black area, 88.0-89.0% in its gray area and 76.9% in its white-gray area), small amount of Si (1.1-2.3%) and residual Cu (4.2-20.8%) coming from the drop detachment. The results of SEM + EDS characterizations suggest that the pancake-like fragment presents the graphene layer detached from the substrate along the substrate/graphene interface and subsequently transferred on the drop surface. Since the diameter of the graphene fragment is comparable to that of the drop/substrate contact area during the first rising of the capillary (about 2 mm), one may conclude that the first upand-down movement of the substrate causes weakening the graphene layer along the contact line. After that the cutting of



Fig. 2 The wetting behavior of Cu drop during wettability test on graphene-coated SiC substrate at 1100 °C (wettability test with alumina capillary): (a) the deposition of the Cu drop; (b) rising of  $C_{Gn}$ /SiC substrate; (c) detachment large solid-like fragment, (d) the end of the test after t = 30 min



**Fig. 3** (a)-(c) Top view SEM images of the Cu drop surface after interaction with the graphene-coated SiC substrate at 1100  $^{\circ}$ C (the wettability test with alumina capillary): (c) and (d) show magnified area of (a) (marked by rectangle) together with corresponding EDS analysis of distribution of Cu, C and Si in points 1-4

graphene layer takes place upon the second substrate lifting and final drop separation from the substrate.

Several combined factors contribute to this phenomenon, e.g., stresses generated from capillary forces at the triple line, the gravitation force, a substrate deformation under acting forces, local defects formed due to the rearrangement of C atoms in the graphene layer in the presence of liquid metal, as well as due to a higher mobility of atoms at high temperature. Moreover, despite a very low solubility of carbon in liquid Cu at the test temperature [ $\sim 1$  at. ppm (Ref 34)], it might be sufficient to create discontinuities in the graphene layer and thus to stimulate its cracking in its most loaded and weakest region corresponding to the contact line.

#### 3.2 Wettability Tests with Graphite Capillary

By taking into account aforementioned considerations, the next wettability tests were performed using a graphite capillary in order to reduce the effect of carbon dissolution in Cu. Based on the Cu-C phase diagram [Fig. 4 (Ref 35)], it was assumed that slow heating of Cu sample in the graphite capillary to the test temperature should cause its saturation with carbon while after melting, the Cu drop might be oversaturated with C. This assumption comes from the peritectic type of the Cu-C system showing that at temperature of peritectic reaction, the solubility of carbon in solid state is much higher as compared to that in liquid state [1.0-7.4 at. ppm (Ref 34, 35) and 10-370 at. ppm (Ref 36, 37), respectively]. The results of recent research (Ref 37) confirmed the maximum solid-state solubility of C in Cu as 10 at. ppm.

During tests with the graphite capillary, two Cu drops were gently deposited on the graphene-coated surface of  $SiC^{sc}$ 



Fig. 4 Cu-C phase diagram (Ref 36)

substrate at 1100 °C as it is shown schematically in Fig. 5. Contrary to previous test with alumina capillary, both drops were easily detached from the graphite immediately after squeezing the molten metal through a hole in the capillary. The detailed analysis of collected images and the corresponding movie (see SUPPLEMENT #2) revealed that within the first second after drop squeezing and deposition (Fig. 6a, b, c, d, e, and f), the first drop only touched the  $C_{Gn}$ /SiC<sup>sc</sup> substrate (Fig. 6b) and then immediately rolled like a ball to another position (Fig. 6c, d, e, and f). After that the drop moved slightly back, and finally it settled near the edge of the substrate, forming asymmetric shape (Fig. 6g and h). During the drop rolling, the change of substrate position and its slight rotation on the alumina support were also noted (as marked by arrows in Fig. 6b, c, d, e, f, and g)



**Fig. 5** A schematic presentation of the sessile drop wettability test of liquid Cu on graphene-coated SiC single-crystalline substrate using the graphite capillary: (a) squeezing of liquid Cu through a hole in the capillary; (b) a gentle deposition of the first Cu drop; (c) a deposition of the second Cu drop after movement of the first drop to the another side of the substrate



**Fig. 6** Images of the first Cu drop recorded with the high-speed high-resolution camera during most representative moments of the first second of the test with the graphite capillary: (a) the start of metal dropping from the capillary—the first drop; (b) touching of the substrate; (c)-(f) the drop rolling; (g) the drop settling; (h) the beginning of test—before second drop squeezing; the arrows indicate the substrate displacement

For the second Cu drop that was dispensed on the same substrate after about 4 s from squeezing the first drop, different wetting behavior was observed (Fig. 7). After the gentle deposition of the second drop on the substrate, rising the capillary caused a short time lifting of the CGn/SiC substrate (Fig. 7a, b, and c). Then the substrate fell down, resulting in the separation of the drop from the capillary, and finally, the drop was settled on the substrate forming a spherical shape (Fig. 7d) without changing its position till the end of the test (Fig. 7f, g, and h). However, contrary to the first drop, a further interaction of the second drop with the substrate was accompanied by the formation of thick interfacial reaction product and the change in the drop size (Fig. 7f). During holding the system at the test temperature for 30 min, notable increase in the volume of reactively formed interfacial region took place at the expense of the decrease in the drop size.

Figure 8(a), (b) and (c) shows the change in contact angle  $(\theta)$  with time during wettability test of two Cu drops on the C<sub>Gn</sub>/SiC<sup>sc</sup> substrate using the graphite capillary. The first Cu drop did not wet the substrate ( $\theta > 90^{\circ}$ ) forming the left and the right contact angles of the same value (121°) at the first

moment of contact with the substrate after squeezing from the capillary (Fig. 8a and b). After settling near the edge of the substrate in about 0.15 s, non-wetting-to-wetting transition took place ( $\theta < 90^{\circ}$ ) and the Cu drop formed the right and left contact angles of different values  $\theta_{\rm R} = 86^{\circ}$  and  $\theta_{\rm L} = 70^{\circ}$ , respectively (Fig. 8b). Whereas the right contact angle was stable with time, the left contact angle started decreasing to form the final value of  $\theta_{\rm L} = 19^{\circ}$  after 30 min. Average value  $\theta_{\rm av} = (\theta_{\rm R} + \theta_{\rm L})/2 = 52^{\circ}$ .

The second Cu drop also did not wet the substrate immediately after its deposition, forming similar right and left contact angles to that of the first drop (123°). However, both angles rapidly decreased in 17 min to the same value of  $\theta = 23^{\circ}$ . A further isothermal heating resulted in the change of the drop shape accompanied with the formation of dissimilar values of right and left contact angle and their increase with time to form an average value of 65° after 30 min.

Besides different wetting behaviors, visual observations of two solidified sessile drops on the same  $C_{Gn}/SiC^{sc}$  substrate (Fig. 9a and b) show their dissimilar shape and size despite of the identical testing conditions. The first drop had an oval shape



Fig. 7 Wetting behavior of the 2nd Cu drop during wettability test on graphene-coated SiC at 1100 °C: (a)-(c) drop deposition; (d) substrate lifting together with raising the capillary; (e) separating of the drop from the capillary; (f) 10 min contact; (g) 20 min contact; (h) the end of the test at time t = 30 min



Fig. 8 The wettability kinetics of liquid Cu on graphene-coated SiC<sup>sc</sup> (the wettability test with the graphite capillary): (a) the first Cu drop; (b) the magnified part of (a) for t = 0.5 s; (c) the second Cu drop



Fig. 9 Macroview images of solidified sessile drop sample showing the first and second Cu drops deposited on the graphene-coated SiC substrate (the wettability test with graphite capillary): (a) the side view, (b) the top view

and from the top view it looks larger than the second drop. Around the first drop, a black oval ring is well distinguished. The second drop has a spherical shape, and it is deep-seated on pyramid with hexagonal base. The surfaces of both drops are bright and occasionally covered with black spots. Moreover, similar black spots are found on the  $C_{Gn}/SiC$  substrate surface near the first drop.

Figure 10, 11, 12, 13 and 14 show the most representative results of SEM examinations of the sample produced during the wettability test with the graphite capillary. Dark spots com-

posed of fine precipitates are well distinguished (Fig. 10a, 11a) on the top views of both solidified drops. They mainly consist of carbon and a small amount of silicon (Fig. 10c, 11c). The side view observations of the first drop revealed many agglomerated dark carbon flakes of different length that reaches the maximum value of 20  $\mu$ m (Fig. 12a and b). Similar regions composed of dark flakes were also detected on the side surface of the second Cu drop (the results are not shown in the paper). On the surface of the first drop displacement path, the presence of gray areas are well recognized (Fig. 13b). In Fig. 14, similar



Fig. 10 (a), (b) Top view SEM images of the first Cu drop surface with marked area in (b); (c) distributions of Cu, C and Si



Fig. 11 (a), (b) Top view SEM images of the second Cu drop with marked area in (b); (c) distribution of Cu, C and Si

areas are also observed near the dark spots shown in Fig. 15. The results of EDS analysis point toward a high content of copper in these dark spots.

Figure 15 shows a comparison of Raman spectra taken from different regions of the examined couple after the wettability

test. Well-distinguished G (1610 cm<sup>-1</sup>) and 2D (2727 cm<sup>-1</sup>) peaks of graphene are found on the spectrum taken from the top surface of the first drop (Fig. 16, spectrum (a) and spectrum (b), respectively). These peaks are much smaller on the spectrum taken from the displacement path of first drop. Moreover,



Fig. 12 (a), (b) Side view SEM images of the first Cu drop surface; (b) marked area in (a) with the results of EDS chemical composition analysis taken from point 1



Fig. 13 (a), (b) Top view SEM images of the first drop displacement path near dark ring formed around the first Cu drop, (c) the distribution of Cu, C and Si



6000 spectrum (a) 5500 5000 4500 4000 Intensity, a.u. pectrum (b) 2D 3500 3000 2500 spectrum (c) 2D 2000 1500 1000 1560 1760 1960 2160 2360 2560 2760 2960 3160 3360 3560 Raman shift, cm<sup>-1</sup>

**Fig. 14** (a) SEM image of spot visible near the black ring and gray area on the SGn/SiC substrate (post-drop rolling region); (b) the results of EDS chemical composition analysis taken from points 1-3 (a)

**Fig. 15** A comparison of Raman spectra at 437 nm excitations and the exposure time of 300 s for: (a) top surface of the first drop; (b) a substrate surface far from the drops; (c) the first drop displacement path on the substrate surface



Fig. 16 Partial pressure of residual gases in the test chamber recorded during experiment with Cu/CGn/SiC couples: (a) RT—before heating; (b) T=200 °C; (c) T=1100 °C—1st Cu dropping; (d) 1100 °C—2nd Cu dropping; (e) T=1100 °C, t=30 min (end of the test)

additional peaks corresponding to SiC appeared, while the FWHM of the 2D peak was 58 cm<sup>-1</sup> corresponding to a bilayer graphene structure (Ref 30). A comparison of the above Raman spectra with those taken from graphene-coated substrate surface far from both drops (Fig. 16, spectrum (c)) suggests the Cu drop displacement on the substrate surface affects its structure and chemistry.

## 4. Discussion

The results of wettability tests of the  $Cu/C_{Gn}/SiC^{sc}$  couples are collected in Table 1 and compared with previous studies of

wetting properties of Cu in contact with different types of SiC substrates (Ref 28-30, 32, 33), graphite (Ref 27, 37), glassy-like carbon (Ref 38), SiO<sub>2</sub> (Ref 39, 40), and SiC substrate coated with graphite layer deposited by ion sputtering ( $C_{dSiC}$ ).

Despite the fact that dissimilar wetting behavior was observed in this research for two Cu drops on graphene-coated SiC single crystal, both drops showed good wetting with the final contact angles of ~ 52° and ~ 65°, for the 1st and 2nd drop, respectively. It is almost three times lower, compared to the contact angle of 157° we observed with liquid Cu on graphite under the same testing conditions but using contact heating (ch) procedure, as reported recently in Ref 38) (Table 1 data "C<sub>gr</sub>"). Moreover, additional test, performed in this study

		Testing conditions			θ, °			
Substrate	Procedure	Atmosphere, p, mbar	T <sub>exp</sub> , °C	Time	Designation	Value	Remarks	Ref.
$C_{Gn}/SiC^{sc}$	cb	vac. 2.18 $\times 10^{-5}$	1100	0 s	$ heta_0$	121.5	1st Cu drop, graphite capillary	This work
				0.15 s	$\theta_{\mathrm{L}}$	86		
				0.15 s	$\theta_{ m R}$	70		
				30 min	$\theta_{\mathrm{av}}$	52		
				0 s	$\theta_0$	123	2nd Cu drop, graphite capillary	
				17 min	$\theta_{17}$	23		
				30 min	$\theta_{30}$	65		
		vac. $2.03 \times 10^{-5}$		0 min	$\theta_0$	112	Alumina capillary	
				30 min	$\theta_{30}$	83		
C <sub>dSiC</sub>		vac. $1.85 \times 10^{-5}$		30 min	$\theta_{30}$	142	Graphite deposited on SiC <sup>sc</sup> by ion sputtering, alumina capillary	
Cer	ch	vac. $1.00 \times 10^{-5}$	1200	30 min	$\theta_{30}$	122	· · ·	Ref 27
2		Ar, $p = 1.0 \times 10^2$	1100	60 min	$\theta_{60}$	157	:	Ref 38
	cb	vac. $1.00 \times 10^{-5}$	1100	n/a	θ	$122 \pm 2$	Pseudo-monocrystalline graphite	dezellus
C <sub>elc</sub>	n/a	n/a	n/a	n/a	θ	136	Cu drop deposited by high-intensity pulsed plasma beam	Ref 39
)	cb	vac. $1.00 \times 10^{-5}$	1100	n/a	θ	$139 \pm 2$		dezellus
SiC <sup>sc</sup>	ch	Ar, $p = 1.00 \times 10^2$	1100	30 min	$\theta_{30}$	130	α-SiC single crystal	Ref <b>33</b>
		vac. $1.00 \times 10^{-4}$	1100	0 min	$\theta_0$	112	α-SiC single crystal	Ref 28
		vac. $1.33 \times 10^{-6}$	1100	n/a	θ	140		Ref 38
SiC <sup>pc</sup>	ch	vac. $1.33 \times 10^{-6}$	1100	30 min	$\theta_{30}$	09	Self-bound $\alpha$ -SiC	Ref 28
		vac. $1.00 \times 10^{-4}$	1100	30 min	$\theta_{30}$	135	Hot-pressed SiC	Ref 29
						83	Reaction bonded SiC	
		vac. $1.00 \times 10^{-5}$	1100	30 min	$\theta_{30}$	140	Pressureless sintered	Ref <b>30</b>
			1200			137		
		Ar, $p = 1.01 \times 10^3$	1150	20 min	$\theta_{20}$	133	α-SiC poly crystal	Ref 32
						137	β-SiC poly crystal	
$SiO_2$	n/a	n/a	n/a	n/a	θ	120-140	SiO <sub>2</sub>	Ref 39
$SiO_2$	ch	$\mathrm{H}_2$	1200	30 min	$\theta_{30}$	118	SiO <sub>2</sub>	Ref 40
Ch contact h	sating techniques	<i>cn</i> canillary murification tec	chniques. C	oranhite $C_{\alpha}$	oranhene C. o	lassw-like carbo	m <i>m</i> nolvervetalline <i>w</i> sincle envetal $C$ carbon denosited on SiC	

Table 1 The contact angles formed at 1100-1200 °C with liquid Cu on different substrates

Table 2 Partial pressure of residual gases in the test chamber recorded during experiment with Cu/C<sub>Gn</sub>/SiC couples

Pressure						
<i>T</i> , time	$P_{\rm H_2}$ , mbar	$P_{\rm H_2O}$ , mbar	P <sub>C</sub> , mbar	$P_{\rm CO+N_2}$ , mbar	$P_{\rm CO_2}$ , mbar	P <sub>total</sub> , mbar
RT	$1.52 \times 10^{-8}$	$2.25 \times 10^{-7}$	$5.93 \times 10^{-10}$	$4.93 \times 10^{-9}$	$7.63 \times 10^{-9}$	$1.2 \times 10^{-6}$
200 °C	$1.64 \times 10^{-8}$	$2.28 \times 10^{-7}$	$7.27 \times 10^{-10}$	$3.85 \times 10^{-9}$	$9.43 \times 10^{-9}$	$1.86 \times 10^{-6}$
400 °C	$6.1 \times 10^{-8}$	$3.29 \times 10^{-7}$	$1.28 \times 10^{-9}$	$6.84 \times 10^{-9}$	$1.65 \times 10^{-8}$	$3.07 \times 10^{-6}$
600 °C	$2.87 \times 10^{-7}$	$4.21 \times 10^{-7}$	$3.89 \times 10^{-9}$	$1.42 \times 10^{-8}$	$5.89 \times 10^{-8}$	$4.75 \times 10^{-6}$
800 °C	$4.62 \times 10^{-7}$	$4.72 \times 10^{-7}$	$7.67 \times 10^{-9}$	$3.4 \times 10^{-8}$	$1.24 \times 10^{-7}$	$6.37 \times 10^{-6}$
1000 °C	$8.3 \times 10^{-7}$	$5.55 \times 10^{-7}$	$1.48 \times 10^{-8}$	$7.93 \times 10^{-8}$	$2.71 \times 10^{-7}$	$1.16 \times 10^{-5}$
1100 °C, $t = 0$ s (1st drop)	$8.3 \times 10^{-7}$	$8.3 \times 10^{-7}$	$5.33 \times 10^{-8}$	$2.94 \times 10^{-7}$	$8.3 \times 10^{-7}$	$2.28 \times 10^{-5}$
1100 °C, $t = 45$ s (2nd drop)	$8.3 \times 10^{-7}$	$8.3 \times 10^{-7}$	$5.24 \times 10^{-8}$	$2.9 \times 10^{-7}$	$8.3 \times 10^{-7}$	$2.18 \times 10^{-5}$
1100 °C, $t = 30 \min$	$8.3 \times 10^{-7}$	$6.54 \times 10^{-7}$	$7.08 \times 10^{-8}$	$4.51 \times 10^{-7}$	$8.3 \times 10^{-7}$	$2.53 \times 10^{-5}$

with liquid Cu on graphite-coated SiC substrate (graphite layer of about 1 micron thickness) using the same testing procedure (non-contact heating) and under the same testing conditions, evidenced only slightly lower contact angle of ~ 142° (Table 1, data "C<sub>dSiC</sub>") (see SUPLEMENT #3), compared to that on bulk graphite.

The comparison of the results of this study with those given in the literature for the Cu/SiC system is much more complicated because literature data are quite scattered and contradict (Table 1). Even for the same testing procedure of contact heating, both wetting and non-wetting were reported, depending on testing conditions and production history of SiC substrates. The highest contact angles of 150° and 130° were observed on polycrystalline B-SiC substrates containing graphite and on pure SiC<sup>pc</sup>, respectively (Ref 33), whereas on SiC single crystal in vacuum of  $p = 1.0 \times 10^{-4}$  mbar contact angle was 112° (Ref 29). The smallest contact angles were observed on polycrystalline reaction-bonded SiC substrates [83° in vacuum of  $p = 1.0 \times 10^{-4}$  mbar (Ref 32) and  $\sim 60^{\circ}$  in a vacuum of  $p = 1.33 \times 10^{-6}$  mbar (Ref 30)]. The highest values of contact angles given in the literature are believed to be related with the effect of SiC oxidation since liquid Cu forms a high contact angle on SiO<sub>2</sub> (120-140° (Ref 39, 40) (Table 1, data "SiO2").

From the first look on the above comparisons, one may suggest that liquid Cu does not recognized the graphene layer because its contact angle on the  $C_{Gn}$ /SiC substrate is most closely comparable to that on SiC than on graphite, hence supporting the graphene wetting transparency effect reported for water (Ref 19). However, in reality the situation is much more complicated and many other phenomena are involved in high-temperature interaction between liquid Cu and graphenecoated SiC. We suggest that the most important one is the rolling of the 1st drop along the substrate surface because it causes: (1) wetting hysteresis and the formation of dissimilar left and right contact angles, (2) detachment of the fragments of graphene layer and their movement to the top of the drop.

Most probably, the observed drop rolling is related with gas release from the substrate as evidenced in real-time records of residual gas analyzer (Table 2, Fig. 16). As shown in Fig. 16(a), just before heating when corresponding vacuum of  $p = 1.20 \times 10^{-6}$  mbar was reached, the low amounts of H<sub>2</sub>O and H<sub>2</sub> were recorded in the chamber. Heating to 200 °C caused only small increase in gasification from the C<sub>Gn</sub>/SiC<sup>sc</sup> substrate (Fig. 16b). However, during further heating to the test temperature of 1100 °C, high amounts of CO<sub>2</sub>, CO, C, H<sub>2</sub>O and

 $H_2$  are released and this effect is accompanied with increase in pressure inside vacuum chamber up to  $p = 2.18 \times 10^{-5}$  mbar, at the moment of squeezing of the 1st drop from the capillary (Fig. 16c). Since dropping the 2nd drop does not change the degree of gasification, we suggest that gas release from the C<sub>Gn</sub>/SiC<sup>sc</sup> contributed to rolling of the Cu drop and its apparently non-wetting behavior.

Comparison of the above results with those of our previous experience shows that the conditions used for substrate storage affect the volume of gases released during heating up to 200 °C (not shown in this study). Similar observations on the release of oxygen and another molecule from graphene-coated SiC during its heating was also reported by Kalbac et al. (Ref 41).

Another reason responsible for unusual behavior of the 1st Cu drop can be related with the changes in the structure and chemistry of the substrate surface during high-temperature heating under UHV. Among others, it can be caused from the difference in the coefficient of thermal expansions (CTE) of graphene  $[-7.0 \times 10^{-6} \text{ K}^{-1} \text{ (Ref 40)}]$  and SiC  $(4.0 \times 10^{-6} \text{ K}^{-1})$ . Kalbac et al. (Ref 41) showed that upon heating to 800 °C, bilayer graphene deposited on SiO<sub>2</sub>/Si by CVD process induces stress due to CTE mismatch of contacting materials and this stress strongly influences the bottom (substrate-side) layer of graphene, whereas its top layer remains almost unaffected. Weis et al. (Ref 42) suggested that it is related with weak bonding between graphene layers subsequently resulting in more pronounced wrinkling of the top layer.

Whatever is the mechanism responsible for the degradation of graphene (cracking due to CTE mismatch, chemical etching by liquid Cu, mechanical detachment by rolling drop), it causes the formation of discontinuities in the layer that in turn accelerates the interaction between liquid Cu and graphene-free SiC. This process is accompanied with (Ref 35): (1) the dissolution of SiC in liquid copper, (2) the formation of interfacial reaction products, and (3) the formation of SiC on the top of the drop (Ref 35).

In this study, the presence of silicon on the surface of both the 1st and 2nd drop has been identified and it presents an experimental evidence of the dissolution of the SiC substrate in liquid Cu. On the other hand, it was observed that the growth of intermediate layer was much slower in the 1st drop than in the 2nd one thus suggesting dissimilar substrate surface conditions for two droplets. Taking into account that the 2nd drop was deposited on postponed area of drop rolling, characterized by weaker signal from graphene, compared to as-received state, we suggest that the contact of graphene layer with the 1st drop and its subsequent rolling resulted not only in reconstruction of graphene layer but even its partial removal from SiC substrate thus making easy further direct interaction between Liquid Cu and graphene-free substrate surface.

Copper does not form any compounds with carbon and it dissolves very little carbon both in solid and liquid states. Therefore, high-temperature interaction in the Cu-C system is widely accepted as non-reactive showing non-wetting behavior and weak Cu-C bonding, independently on the allotropic form of carbon, such as graphite (Ref 10), glassy-like carbon (Ref 11), diamond (Ref 12), carbon fibers (Ref 13).

The acceleration of reactivity in the Cu/SiC system is affected by the presence of pristine SiC surface (after removing graphene layer). Absence of SiO<sub>2</sub> normally present on the surface of SiC monocrystals was due to the sublimation method by which graphene was produced. The said method consists in a sublimation of Si from the surface under the conditions of UHV and high temperature (Ref 43). Carbon undergoes rearrangement to form a layer of graphene, which acts as a barrier to the SiC substrate oxidation. That indicates that the layer of graphene under the 2nd Cu drop was totally degraded and was not a barrier to mass transport as for 1st Cu drop whose intermediate layer was much thinner.

Another experimental evidence of absence of graphene layer in the place where the second drop was deposited is the hexagonal shape of a solid-like interface formed under second droplet. The appearance of the solid-like interface as a pyramid with hexagonal base shape has revealed that the reaction of Cu with substrate is controlled solely by the crystallographic nature of  $\alpha$ -SiC (Ref 31).

Therefore, it cannot be excluded that under the conditions of our experiment, a similar phenomenon might have happened between graphene with liquid Cu: (1) destruction of graphene layer by C dissolution in Cu; (2) growth of graphene on molten Cu drop surface.

Although the dissolution of C in molten Cu is extremely low (0.02 at.%) (Ref 41, 44) and molten Cu was saturated in graphite capillary, the partial or complete dissolution of graphene cannot be entirely excluded. Fuks et al. showed that after heat treatment even at 1000 °C by 1 h, Cu reacted with C and the Cu-C solid solution of 50 nm thickness was formed (Ref 44).

The partial or complete dissolution of graphene promotes dissolution of SiC in Cu in discontinuities. The dissolved SiC becomes additional C source for the formation of a new layer of graphene on Cu surface.

The presence of uniform double-layered graphene (Ref 45) on the 2nd Cu drop surface revealed in Raman spectra suggests that it could be obtained by means of growth of graphene sheets on liquid Cu.

A uniform hexagonal graphene flakes growth on liquid Cu drop at 1080 °C under  $CH_4$  flow was reported by Geng et al. (Ref 46). They demonstrated that the use of molten Cu is particularly effective means for controlling the nucleation process in graphene CVD synthesis and results in the production of uniform, single-layered, self-aligned, large-sized, single-domain graphene sheets and continuous monolayer film. Therefore, it cannot be excluded that during graphene formation, an additional process could occur, mainly re-knitting of sheets.

The pieces of the graphene layer detached from SiC surface layer (mechanical detaching by the 1st drop) can flow on the

top surface of Cu drop where it can react with single carbon atoms (from dissolved SiC, graphene or graphite capillary) forming new graphene sheets. During this process, the selfhealing of graphene sheets can occurs.

Similar self-healing process was described by Zan et al. (Ref 47) who observed that in the presence of metal, graphene can be etched on the nanoscale under. This phenomenon is accompanied by either knocking of carbon atoms out from neighboring edges or supplying by nearby hydrocarbon contamination patches.

A number of various phenomena can occur at the same time, wherefrom it follows that clarification of the wetting behavior of graphene in contact with molten Cu requires additional research.

# 5. Conclusions

Studies of the interaction between liquid metal and graphene-coated monocrystalline SiC substrate are characterized by high degree of intricacy and require special methods and procedures developed in order to test the specific nature of interactions between 2D materials at high temperature. The tests made with liquid Cu at 1100 °C confirm the complexity of interactions, evidenced also during tests with liquid Sn carried out at 350 °C (Ref 20).

The behavior of the Cu drop in few attempts to detach it from the graphene-coated SiC substrate by rising up a graphite capillary showed a strong adhesion of the liquid Cu to the SiC. Similar behavior of the Cu drop took place with graphene-free SiC substrate, while with graphite substrate, the Cu drop was easily detached without raising the substrate. These observations can be considered as indirect experimental evidence of the wetting transparency of graphene layer for liquid Cu.

The results of SEM investigations and Raman spectroscopy studies suggest that the presence of graphene layer on the SiC substrate suppresses but does not completely prevent chemical interaction between liquid Cu drop and SiC. Both chemical degradation (etching) and mechanical degradation of the graphene layer are responsible for the formation of discontinuities in the graphene layer. This in turn resulted in mass transfer through the interface and in changes of structure and chemistry of the drops and the interfaces formed. This effect is more pronounced for the second drop deposited on the path made by the first drop after its rolling.

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