

Article

# Mechanical Properties of Monolayer MoS<sub>2</sub> with Randomly Distributed Defects

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Received: 17 February 2020; Accepted: 10 March 2020; Published: 13 March 2020



**Abstract:** The variation of elastic constants stiffness coefficients with respect to different percentage ratios of defects in monolayer molybdenum disulfide (MLMoS<sub>2</sub>) is reported for a particular set of atomistic nanostructural characteristics. The common method suggested is to use conventional defects such as single vacancy or di vacancy, and the recent studies use stone-walled multiple defects for highlighting the differences in the mechanical and electronic properties of 2D materials. Modeling the size influence of monolayer MoS<sub>2</sub> by generating defects which are randomly distributed for a different percentage from 0% to 25% is considered in the paper. In this work, the geometry of the monolayer MoS<sub>2</sub> defects modeled as randomized over the domain are taken into account. For simulation, the molecular static method is adopted and study the effect of elastic stiffness parameters of the 2D MoS<sub>2</sub> material. Our findings reveals that the expansion of defects concentration leads to a decrease in the elastic properties, the sheer decrease in the elastic properties is found at 25%. We also study the diffusion of Molybdenum (Mo) in Sulphur (S) layers of atoms within MoS<sub>2</sub> with Mo antisite defects. The elastic constants dwindle in the case of antisite defects too, but when compared to pure defects, the reduction was to a smaller extent in monolayer MoS<sub>2</sub>. Nevertheless, the Mo diffusion in sulfur gets to be more and more isotropic with the increase in the defect concentrations and elastic stiffness decreases with antisite defects concentration up to 25%. The distribution of antisite defects plays a vital role in modulating Mo diffusion in sulfur. These results will be helpful and give insights in the design of 2D materials.

**Keywords:** mono-layer MoS<sub>2</sub>; mechanical properties; molecular statics/dynamics; defects; random distributed defects

## 1. Introduction

The early reports on graphene by Giam [1], specifically considering two dimensional (2D) materials like transition metal dichalcogenide (MX<sub>2</sub>, M = Mo, W; X = S, Se, Te), or particularly Monolayer MoS<sub>2</sub> (MLMoS<sub>2</sub>) have lure in the applications of electronics to structural and functional composites [2–5] owing to its exceptional electrical, optical, and mechanical properties. In structural applications, the most appealing feature of MoS<sub>2</sub> is the in-sheet elastic stiffness of perfect sp<sup>3</sup> covalently bonded structures [6,7]. Two dimensional MoS<sub>2</sub> is tri-layer as opposed to graphene, which is only single-layer, monolayer MoS<sub>2</sub> having a system of three atomic thickness layers with the transition metal (Mo)

atomic layer clogged in the intermediate of two S atom layers [8]. Deji Akinwande [9] reported recent studies related to mechanics, which include interfacial properties and a combination of mechanical and physical properties of 2D materials from both theoretical and experimental aspects. Kai Liu et al. [10] reported the effect of defects on the mechanical properties of graphene and 2D transition metal dichalcogenides, with the elastic properties measured by the experimental nanoindentation technique. Several researchers [11–14] study the mechanical properties and its effects of defects in MoS<sub>2</sub> structure, which captures the geometrical aspects of the defects of diverse defect concentrations. It is driven by the simple fact experimentally measured elastic strengths of MoS<sub>2</sub> significantly corresponds to theoretical expectations for the defect-free structures, and that they exhibit a significant statistical scatter [15]. Theoretical investigations of defected MoS<sub>2</sub>, Li et al., have mainly focused on molecular dynamics (MD) simulations [16], with VMoS<sub>3</sub> defects using Reactive Empirical Bond Order (REBO) potential. Spirko et al investigated the defects of MoS<sub>2</sub> structure using DFT method [17]. Wang et al. [18] reported the monolayer MoS<sub>2</sub> with sulfur vacancy mechanical response under tensile load for electronic and structural properties studied by using first-principles calculations. Besides investigations of the result of single defects, like few studies, Stone–Wales defects and vacancies have addressed the effect of multiple randomly distributed defects. Multiple defects will not just result in a decrease in strength due to microcrack interactions, but might also give rise to a significant scatter in strength related with statistical size effects as larger samples have an enhanced probability to contain weak local configurations. Both experiments [11] and simulation [16] indicate that the strength distribution of MoS<sub>2</sub> with multiple defects well described by Weibull statistics and exhibit the typical size effects characteristic of weakest link controlled failure. Similar investigations have been conducted in the previous work for MoS<sub>2</sub> [14,16,18].

Samaneh Nasiri [19] investigated the statistical failures analysis in graphene monolayer considering random defects distribution by varying both size and defects concentration. Liu Chu et al. [20] also investigated the effects of random vacancy defects and the tendency due to elastic buckling in single-layer graphene. To this end, chalcogen atoms, i.e., sulfur is the common form of vacancies formed in the TMDs. Shanshan Wang et al. [21] described how sulfur atomic loss is prevalent in MoS<sub>2</sub> structure and can occur in both top and bottom layers. J.A. Stewart [22] conducted molecular statics nanoindentation on MoS<sub>2</sub>, which leads to phenomena of structural deformation by classical molecular simulations. Electronic structures and elastic properties, in particular, elastic constants of MoS<sub>2</sub> under pressure conditions, have been examined via first-principle calculations by Li Wei et al. [23]. Lattice defects were introduced by Yan Chen [24] in monolayer MoS<sub>2</sub> by thermal annealing in a vacuum and by Ar<sup>+</sup> ion irradiation. He reported that defects play an influential role in forming the electronic structure by both approaches and the information of defects which can alter the properties of MoS<sub>2</sub>. He introduced lattice defects in monolayer MoS<sub>2</sub> by both thermal annealings in a vacuum and by Ar<sup>+</sup> ion irradiation. It has revealed the electronic structure influenced by the lattice defects formed in those ways by both approaches. This information helps to interpret the mechanisms by which the defects alter the properties of MoS<sub>2</sub>. Independent elastic constants by using density functional theory are well described by Nguyen T. Hung [25] as they concentrate on electromechanical properties both 1H and 1T MoS<sub>2</sub> monolayer as a role of charge doping.

Generally, atomistic simulation packages use the minimum energy configuration to determine the strength of the structure under load, and this is strated by using the conjugate gradient minimization. This minimization gives knowledge about crystal lattice structure in different phases and under different conditions. Molecular static simulations examine the mechanical properties, especially independent elastic constants of monolayer Molybdenum disulfide (MLMoS<sub>2</sub>) containing point defects, like vacancies of Sulphur (S) atoms. In this paper, the defects in the monolayer MoS<sub>2</sub> are entirely random, and modeling such complex random defects performing many simulations run with molecular statics does capture the elastic constants properties correctly. In this method, each run of the defects simulation with varying defect fraction from 0% to 25%, and for each defect fraction, the elastic properties captured were most of the topological aspects of the monolayer nanosheet. Li et al. and

Wang et al. [16,18] proposed the low concentration defects on the topology, whereas we reported for defects varying from low to high concentration to mimic the mono-layer topology in MoS<sub>2</sub>. This method requires multiple defects with the varying defect concentration on the topology generated by using conventional molecular static modeling, namely topology-based atomistic defects caused by using random equilibrium distribution of the domain utilized in this study. Jinhua Hong et al. [26] pointed out that antisite defects with replacing molybdenum as sulfur, which are prevalent point defects in PVD-grown MoS<sub>2</sub>, while the sulfur vacancies are predominant in mechanical exfoliation and CVD specimens in MoS<sub>2</sub>.

The MoS<sub>2</sub> is also interesting due to the electrical, thermal, and optical properties. The paper [27] presents results of influence of vacancies on electrical properties of MoS<sub>2</sub>, this work focuses on studying the mechanical properties of monolayer MoS<sub>2</sub> with randomly distributed defects by systematically varying the vacancy concentration, The new results obtained for different levels of defects are presented. The results are shown for different random defect distributions. The results may be used in future works were the mechanical nanomachines and nanosystems based on MoS<sub>2</sub> sheets optimization are considered. The simulation methodology is detailed in Section 2.1, while the theoretical framework used for defectcted sheet analyzing is defined in Section 2.2. Results are presented in Section 3, and discussion and conclusions are presented in Section 4.

## 2. Materials and Methods

### 2.1. Methodology of Molecular Simulations

This study investigate the mechanical properties of pristine and defective monolayer MoS<sub>2</sub> structure including the relaxation strcutre through molecular static simulations and the calculations are performed in atomistic based LAMMPS (Large-Scale Atomic Molecular Massive Parallel Simulator, Sandia National Laboratories, Albuquerque, USA) [28,29], open source package developed by Sandia National Laboratories to model. The heart of the molecular simulations is the inter-atomic potential, which applies to describe the interaction among atoms. From the inter-atomic potential, we can obtain the new properties of any material like theoretical strength, elastic moduli, and Hooke's law. Stillinger–Weber (SW) potential employs an effective approach to describe the interactions in MoS<sub>2</sub> by considering all possible interactions between Mo and S [30–32].

To understand all its physical properties and know how to control these properties for specific usage, one needs to know the accurate interatomic potential. The potential used in our simulation representing Mo and S atoms developed by Stillinger–Weber (SW) potential of MoS<sub>2</sub>, which includes all possible interactions Mo and S [30,31] as it is a many-body potential (the potential consists of one-,two- and three-body terms) which perfectly fitted to mono-layer MoS<sub>2</sub>. In this work, we performed molecular static (MS) simulations to generate the elastic constants of the monolayer MoS<sub>2</sub>. The parameters used in the simulation will influence the accuracy of the computed results. Consequently, we used the well parameterized molecular simulation that can describe the variety of bulk material properties. The bond interaction by two-body interaction acts towards the bond deformation while the three-body interaction conducts itself towards the angular rotation. The total potential of a system  $\varphi_{tot}$  can be written as

$$\varphi_{tot} = \sum_i \sum_{i < j} Q_2(r_{ij}) + \sum_i \sum_{j \neq i} \sum_{k > j} Q_3(r_{ij}, r_{ik}, \alpha_{ijk}) \quad (1)$$

The two-body interaction potential  $Q_2$  takes the following form.

$$Q_2(r_{ij}) = X_{ij} \left( \frac{Y_{ij}}{r_{ij}^4} - 1 \right) e^{\left( \frac{\alpha_{ij}}{r_{ij} - r_{ij}^{max}} \right)} \quad (2)$$

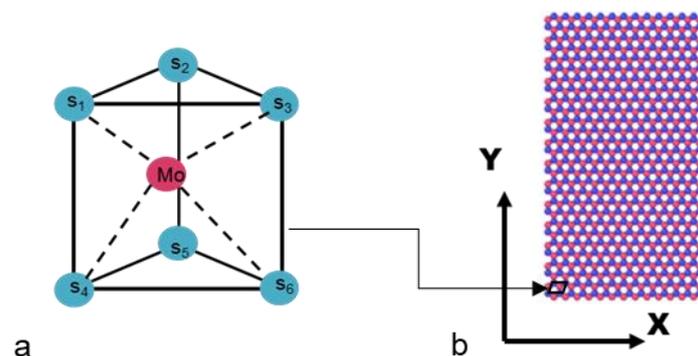
The three-body interaction potential  $Q_3$  in Equation (1) is modeled as

$$Q_3(r_{ij}, r_{ik}, \alpha_{ijk}) = Z_{ijk} e^{\left(\frac{\sigma_{ij}}{r_{ij}-r_{ij}^{max}} + \frac{\sigma_{ik}}{r_{ik}-r_{ik}^{max}}\right)} \times (\cos \alpha_{ijk} - \cos \alpha_{0,ijk})^2 \quad (3)$$

where exponential function gives a smooth decay of the potential to zero at the cut-off, which is essential to save the energy.  $Q_2$  and  $Q_3$  represents the two body (bond stretching) and three body (bond bending) interactions. The  $r_{ij}$ ,  $r_{ik}$  and  $\alpha_{ijk}$  are the pair separations and angle between the separation on atom  $i$  respectively. The potential parameters are  $X$ ,  $Y$ ,  $Z$ ,  $\sigma$ , along with  $r^{max}$  cutoff radii and equilibrium angles and they rely upon on the atoms interacting with each other, for instance,  $X_{ij}$  is the parameter for  $X$  for the pairwise interaction between atom  $i$  of category  $I$  and atom  $j$  of category  $J$ .

## 2.2. Crystal Structure

A cubic domain of monolayer  $\text{MoS}_2$  with 1000 atoms was generated using LAMMPS is shown in Figure 1. The crystal orientation was aligned in order that all three principal directions of the crystal align with global coordinate system. The domain has  $4.74 \times 8.21 \times 0.615$  nm which is equal to  $15a \times 15a \times 1a$ , as shown in Figure 1b. The atomistic model in the present work is developed by considering the hexagonal lattice structure of  $\text{MoS}_2$  sheet with the lattice constant of  $a = 3.16$  Å and  $c = 6.15$  Å. The main objective of this work is to understand the topology of defects by varying size of domain. After the sheets had been relaxed over sufficiently long period of time by conjugate gradient optimization till the energy is conserved. The mechanical properties of  $\text{MoS}_2$  are estimated in the next section.



**Figure 1.** (a) Unit cell of hexagonal  $\text{MoS}_2$  (b)  $15a \times 15a \times 1a$   $\text{MoS}_2$  bulk structure (S = Blue or light; Mo = Purple).

The atomic model consists of 25,000 atoms in the nanosheet for the domain size of  $12.95 \text{ nm}^2$  to  $56.11 \text{ nm}^2$ . In this work for each simulation, the initial configuration of the  $\text{MoS}_2$  sheet was prepared, and the random defects were introduced. The periodic boundary conditions in all directions were enforced, and monolayer  $\text{MoS}_2$  sheets with  $65 \times 65 \times 1$  lattices are presented in the results section. Point defects (vacancies) are created by randomly removing atoms with probability from the lattice sites. The vacancies or defects are randomly placed in the crystal using a random number generator with uniform distribution. Defect concentrations range from  $Vc = 0.01\%$  to  $25\%$  are considered. Hundreds of simulations were performed for each vacancy concentration with different defects locations.

In this work, to see the antisite defects, in particular, the molybdenum (Mo) atoms diffusing in sulfur layers with an assortment of random defect concentrations with different configurations is chosen. There were 5, 56, 120, 296, 571, 867, 1143 and 1427 atoms of molybdenum antisite defects in the  $\text{MoS}_2$  sheet that contains 25,000 atoms, which stand for a defect concentration of 0.1%, 1%, 2%, 5%, 10%, 15%, 20%, and 25%, respectively. Local structures and diffusion dynamics have a significant influence on the interaction of defects for significant defect fraction ratios. Thus, we explore the impact of antisite defects in  $\text{MoS}_2$ .

### 2.3. Elastic Constants of Monolayer MoS<sub>2</sub> Using Molecular Statics (MS)

Molecular statics calculations have been performed using LAMMPS code to generate the elastic constants of MoS<sub>2</sub> at 0 K. We know that the MoS<sub>2</sub> sheet consists of a tri-layer, and it experiences strong covalent bonding inward and weak van der Waal's interaction over the tri-layer due to the polarization effect [22]. The elastic properties of MoS<sub>2</sub> are determined as the derivative of the stress against the external strain according to Hooke's law. The generalized Hooke's law, for the number of independent elastic constants in MoS<sub>2</sub>, is three and can be written as

$$\sigma_{ij} = C_{ij}\varepsilon_{ij} \quad (4)$$

There are three independent elastic constants for MoS<sub>2</sub>, i.e.,  $C_{11}$  is the coefficient of elastic constant relations due to  $\sigma_{11}$  to  $\varepsilon_{11}$  similarly for  $C_{22}$ , and  $C_{12}$ . The  $C_{ij}$  values are correlated to the equal volume of the MoS<sub>2</sub> unit cell. Therefore, the vacuum space has been set up large enough in the z-axis to avoid the interlayer interactions in MoS<sub>2</sub> monolayer; the  $C_{ij}$  constants then have to rescaled  $z = t_0$  to the actual thickness of monolayer MoS<sub>2</sub>. So, we have set  $t_0 = 6.15 \text{ \AA}$ , i.e., one half of the out-of-plane lattice constant of bulk MoS<sub>2</sub>. The MoS<sub>2</sub> structure is fully optimized to its minimum energy by conjugate gradient minimization until the energy is converged. The specific finite lattice distortion of the simulation box leads to a change in energy during convergence, and the respective final elastic constants are obtained [33,34].

The second-order elastic constants for elastic matrix express as:

$$C_{ij} = \frac{1}{S_0 t_0} \left( \frac{\partial^2 E}{\partial \varepsilon_i \partial \varepsilon_j} \right) \quad (5)$$

where  $S_0$  is the area of the sample,  $t_0$  represents the thickness of MoS<sub>2</sub> monolayer,  $E$  is the elastic energy, and  $\varepsilon$  is the strain tensor. In polynomial form for 2D materials discussed in [34,35], the elastic energy  $E(\varepsilon)$  of MoS<sub>2</sub> is expressed as:

$$E(\varepsilon) = \frac{1}{2} C_{11} \varepsilon_{xx}^2 + \frac{1}{2} C_{22} \varepsilon_{yy}^2 + C_{12} \varepsilon_{xx} \varepsilon_{yy} + 2\varepsilon_{66} \varepsilon_{xy}^2 \quad (6)$$

The  $\varepsilon_{xx}$  and  $\varepsilon_{yy}$  are the longitudinal strain in  $x$  and  $y$  directions and can also be represented as  $\varepsilon_1$  and  $\varepsilon_2$  respectively in terms of Voight notations, and  $\varepsilon_{xy}$  is the applied shear strain in  $xy$  plane. The MoS<sub>2</sub> sheet is arranged as zigzag and armchair in the  $x$  and  $y$ -axis.  $\varepsilon_{ij}$ 's and  $C_{ij}$ 's are the corresponding infinitesimal strain tensors and linear elastic constants [34,36]. Born set the benchmark mechanical stability for graphene-like 2D materials, which explains  $C_{11} > 0$ ,  $C_{11} > C_{12}$ , and  $C_{12} > 0$  and the condition to satisfy for the 2D materials to be isotropic is  $C_{11} \approx C_{22}$  and  $C_{12}$ . The elastic energy in general for 2D materials for finite distortion is expressed as

$$E(\varepsilon) = \frac{1}{2} (\varepsilon_1 \varepsilon_2, 2\varepsilon_6) = \begin{pmatrix} C_{11} & C_{12} & 0 \\ C_{21} & C_{22} & 0 \\ 0 & 0 & \frac{C_{11}-C_{12}}{2} \end{pmatrix} \begin{pmatrix} \varepsilon_1 \\ \varepsilon_2 \\ 2\varepsilon_6 \end{pmatrix} \quad (7)$$

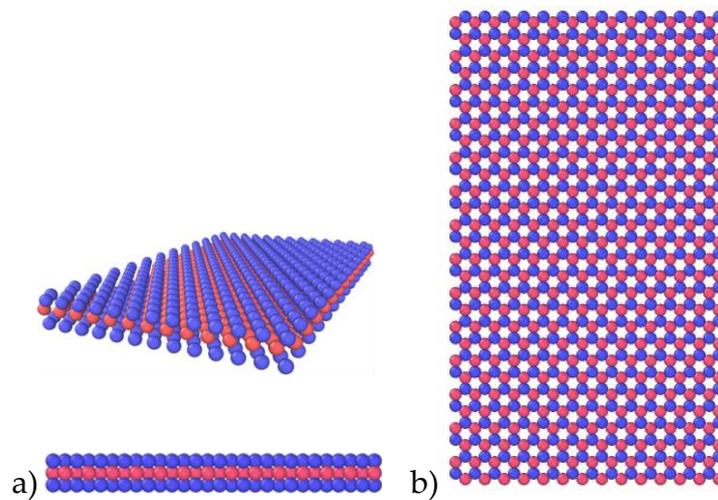
After the MoS<sub>2</sub> sheet is perfectly relaxed or energy is fully converged, the independent elastic constants are extracted for respective strains.

## 3. Results and Discussion

### 3.1. MoS<sub>2</sub> Sheet with Pristine and Random Vacancy Defects

Our findings shows that the elastic constants for a MoS<sub>2</sub> sheet with an infinite system size are  $C_{11} = C_{22} = 149.42 \text{ N/m}$ ,  $C_{12} = 52.29 \text{ N/m}$ , which interpret the isotropic nature of the material. One

such example of MoS<sub>2</sub> microstructure with no defects is shown in Figure 2. Open Visualization Tool (OVITO) [37] was used for the visualization of results.



**Figure 2.** The atomistic model of monolayer MoS<sub>2</sub> without defects, blue balls represents Sulphur atoms top and bottom layers and red balls represent Molybdenum. The elastic constants for this pristine MoS<sub>2</sub> are  $C_{11} = C_{22} = 149.42$  N/m,  $C_{12} = 52.29$  N/m. (a) Side and isometric view (b) top view.

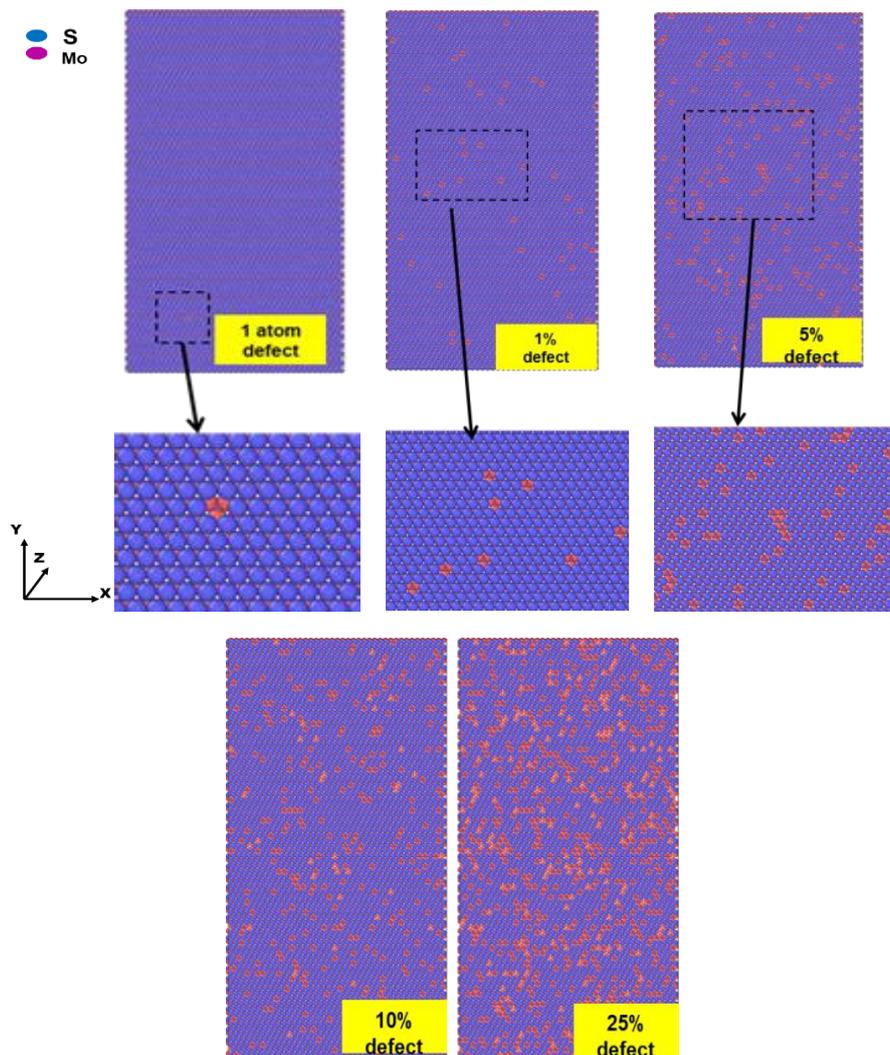
Since the independent elastic constants for a 2D material MoS<sub>2</sub> are five within the notation employed, the constant elastic tensor is a  $3 \times 3$  symmetric matrix. Due to symmetry, some components vanishes and the elasticity matrix elements will get reduced to three independent elements. The calculated elastic constants of MoS<sub>2</sub> are shown in Table 1.

**Table 1.** The material properties of MoS<sub>2</sub>.

CODE	$C_{11}$ [N/m]	$C_{22}$ [N/m]	$C_{12}$ [N/m]
This work	149.42	149.42	52.29
Bertolazzi et al. [8]	$180 \pm 60$	$180 \pm 60$	–
Li. M. et al. [19]	148.4	148.4	42.9
Nguyen T.H. et al. [28]	130.4	130.4	26.5

All elastic constants  $C_{ij}$  calculated by conjugate gradient minimization using molecular statics simulation in comparison with literature results are given in Table 1. Due to symmetry  $C_{11} \approx C_{22}$  the obtained elastic constants marginally diverse from the reference data. We can see that  $C_{11} = 149$  N/m, which corresponds to a good Young's modulus of 242 GPa. Bertolazzi et al. [5] reported the elastic stiffness of MoS<sub>2</sub> monolayer is  $180 \pm 60$  N/m, which corresponds to a good Young's modulus of  $270 \pm 100$  GPa by the atomic force microscope (AFM) experiment method. The experimental results are higher than our simulation results from this study because in AFM method, tip enforced on the sheet consists of monolayer or multilayer MoS<sub>2</sub> suspended on the layer incorporate with an array of circular holes are under biaxial tensile stress whereas we have applied uniaxial stress to the monolayer. Li et al. [16] performed MD simulation under the uniaxial test presented that  $C_{11}$  is found to be 199 GPa for the 1H MoS<sub>2</sub>, our results are while Nguyen T.H. [25] obtained an average young's modulus of 201 GPa for monolayer MoS<sub>2</sub>. Note the deviation due to the performed DFT calculations, which are derived from the finite difference approach by Thermo-pw code, and we have used latest SW potential which can be used for higher temperatures as well. A comparison of elastic constants from this work are consistent with the experimental and simulation results. Regardless of vacancies, the average value of  $C_{12}$  and  $C_{21}$  is used to assess the physical properties of MoS<sub>2</sub>. It is apparent that  $C_{12} \approx C_{21}$  due to the symmetric stiffness matrix.

We now describe the effects of modeling monolayer MoS<sub>2</sub> sheet with randomly distributed defect fraction presented in Figure 3. The geometry optimized average elastic constants for MoS<sub>2</sub> under different defect fractions are given in Table 2. The elastic constants of monolayer MoS<sub>2</sub> vs. the defect percentage are illustrated in comparison to the perfect MoS<sub>2</sub> sheet. The MoS<sub>2</sub> monolayer sheet is arranged as zig-zag and armchair in *x* & *y* directions, which denotes the  $C_{11}$ ,  $C_{12}$ , and  $C_{22}$  elastic moduli, respectively. It is clear that chirality slight effect on elastic constants irrespective of defect ratios. The elastic constants  $C_{ij}$  nonetheless started dwindling as the defect fraction piled up from 0% to 25%. Its reduction becomes more expeditiously as the defects grow in the sheet. Piling up the defect fraction and maximum ratio up to 25% results in a considerable decline in the elastic constants, which implies the impact is significant.

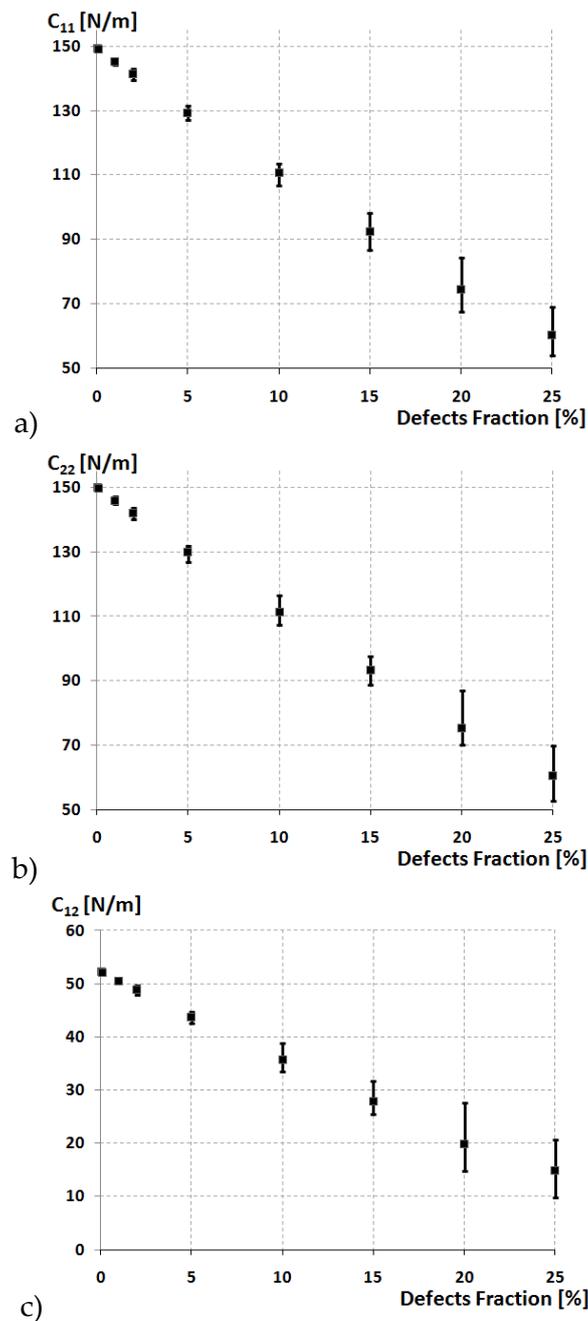


**Figure 3.** The atomistic model of monolayer MoS<sub>2</sub> with different percentage of defects.

The elastic constants of monolayer MoS<sub>2</sub> nanosheet vs. the defect percentage are presented in Figure 4. The dots denote average values of defects fraction with the fluctuating bar represents the standard deviation that shows maximum and minimum values for hundreds of cases with random distributed defects. The result of chirality on the elastic properties of MoS<sub>2</sub> is negligible, despite the prevailing circumstances of the defect fraction. The elastic constants dwindle faster with the increase in the defect fraction, the maximum reduction of elastic constants is at 25%, more significant than 15%, 10%, and 5%, which implies the influence of defect fraction on the elastic constants is found to be substantial.

**Table 2.** The mechanical parameters for MoS<sub>2</sub> for different defect fractions along with Standard Deviation (SD).

% of Defects	$C_{11}$ [N/m]	SD ( $\sigma_{C11}$ )	$C_{22}$ [N/m]	SD ( $\sigma_{C22}$ )	$C_{12}$ [N/m]	SD ( $\sigma_{C12}$ )
Pristine MoS <sub>2</sub>	149.42		149.42		52.29	
Only 1-atom defect	149.11	0.1070	149.04	0.1075	52.23	0.0460
1%	149.01	0.4758	148.85	0.4935	52.15	0.2185
2%	140.70	0.7898	141.51	0.7638	48.52	0.3836
5%	128.89	1.0179	128.89	1.1328	43.25	0.5485
10%	108.30	1.5842	107.94	1.7279	33.70	1.0182
15%	94.21	2.2419	93.47	2.2325	28.75	1.4486
20%	80.99	3.5597	78.46	3.2201	23.16	2.4461
25%	61.15	3.2207	51.52	3.2868	10.67	2.2325

**Figure 4.** The elastic constants of MoS<sub>2</sub> as a function of the defect fraction: (a)  $C_{11}$ , (b)  $C_{22}$ , (c)  $C_{12}$ .

To give comprehensive and comparable studies of elastic properties of randomly distributed defects, the elastic constants of MoS<sub>2</sub> with varying defect ratios have been studied. The elastic constants of this defective MoS<sub>2</sub> versus defect fraction are shown in Figure 4. For comparison, the elastic constant of pristine MoS<sub>2</sub> also included in the plots. Figure 4 shows the effect of defects on the elastic constants of MoS<sub>2</sub> along with the individual independent elastic constants by comparing that of the pristine MoS<sub>2</sub>. It will be hard to conclude the locations of the unperturbed vacancies as they are distributed randomly throughout the layer. We took an interest in determining that these vacancies need to form everywhere in the sheet, irrespective of defect fraction ratio. So, to achieve this, we repeated with different random seeds for a sufficient number of times and estimated the elastic constants for each seed.

Table 2 displays the average values of the outcomes of the built-in elastic test after repeating the simulation. These results will also motivate us to study the tensile and other properties of MoS<sub>2</sub> with the defects. With the increase in defect ratio, we observe the difference in the elastic constants nonlinearly as expected. It was found that up to 1% of defects had little impact as it trims down to 2.1% rate of elastic constants when compared to defect-free MoS<sub>2</sub> and the impact of this vacancy defects on the elastic constants was not that obvious and can be neglected. When the defect fraction surpasses 2%, the elastic constants start trimming down at a rapid rate. Nevertheless, when defect ratios was 2%, 5%, 10%, and 25%, the decrease of the elastic constants was 4.02%, 13.42%, 28.8%, and 56.5%, respectively, compared with MoS<sub>2</sub> with no defects. This result showed that after exceeding some defect density, the vacancy had a substantial effect and damages the robustness and uniform symmetry of MoS<sub>2</sub> and has a full impact on the elastic tensile behavior of MoS<sub>2</sub>. It was also found that from Figure 4 as the elastic constants fluctuate within a certain range, and this fluctuation occurs due to the locations of the defects placed randomly and changes its location with each test. These results draw attention towards the foundation in randomly distributed vacancies in MoS<sub>2</sub> sheets.

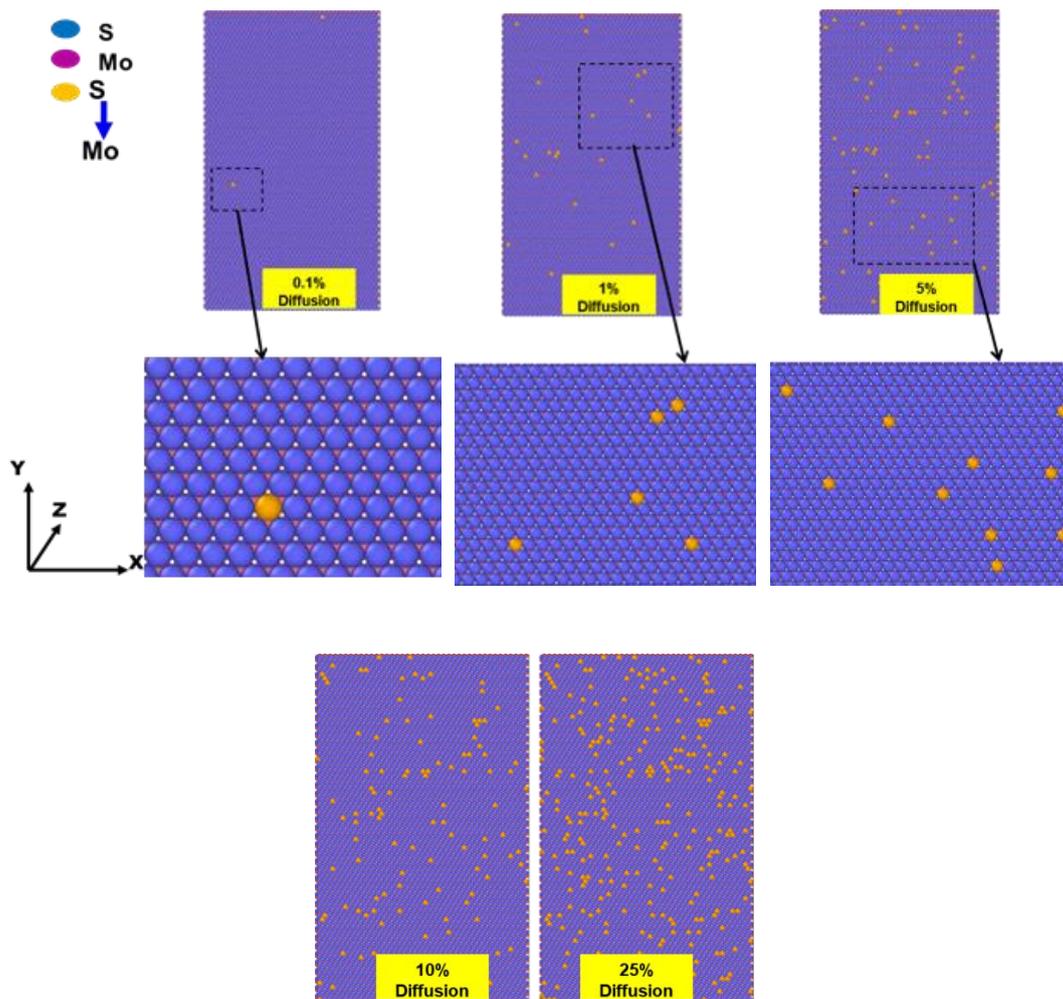
### 3.2. MoS<sub>2</sub> Sheet with Randomly Diffusing Sulfur to Molybdenum (S→Mo)

The concentration of antisite defects, i.e., sulfur atoms to molybdenum atoms, are also randomly distributed in sulfur layers of the MoS<sub>2</sub> sheet. Figure 5 shows the diffusion of sulfur to molybdenum as antisite defect for different percentages of sulfur diffused in monolayer MoS<sub>2</sub> for 25000 atoms nanosheet size. Table 3 shows that the elastic stiffness strengths of 0% to 25% molybdenum doped in sulfur layers in monolayer MoS<sub>2</sub> for sheet size of 65 Å × 65 Å (25000 atoms) increase by about 0.1%, 2%, 1%, 5%, and an impressive peak of 25% when compared with the MoS<sub>2</sub> is observed.

**Table 3.** The geometry optimized structural parameters for MoS<sub>2</sub> for different defect fractions of antisite defects along with Standard Deviation (SD).

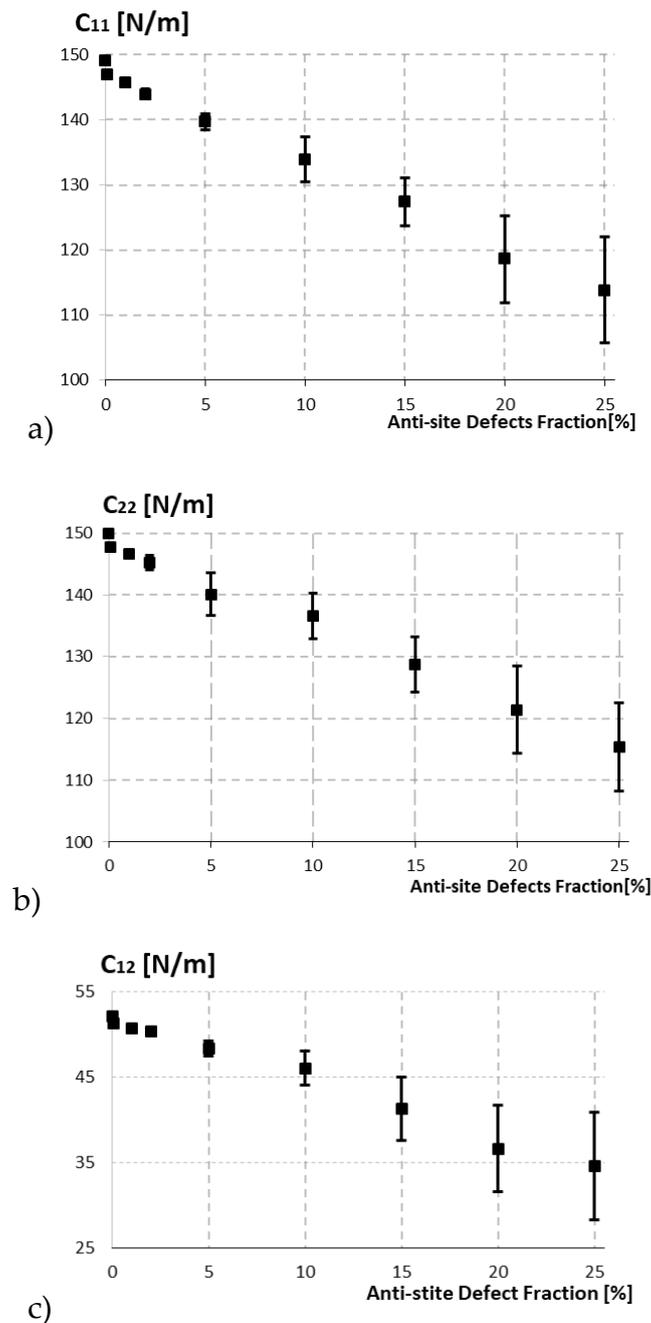
% of Diffusion	C <sub>11</sub> [N/m]	SD (σ <sub>C11</sub> )	C <sub>22</sub> [N/m]	SD (σ <sub>C22</sub> )	C <sub>12</sub> [N/m]	SD (σ <sub>C12</sub> )
0% w/o diffusion	149.42		149.42		52.14	
0.1% S→Mo	147.03	0.0996	147.77	0.2300	51.29	0.0658
1% S→Mo	145.82	0.3224	146.60	0.5541	50.77	0.1621
2% S→Mo	143.98	0.4166	145.24	0.5991	50.38	0.1886
5% S→Mo	139.69	0.6203	140.10	0.6698	48.39	0.2296
10% S→Mo	133.91	0.8259	136.61	0.9077	46.04	0.2725
15% S→Mo	127.40	0.9695	128.76	0.9829	41.25	0.3107
20% S→Mo	118.75	0.9553	121.41	0.9556	36.62	0.3009
25% S→Mo	61.15	1.016	51.52	0.9981	10.67	0.3607

The independent elastic constants of 1%, 2%, 5%, 10%, as well as 15% sulphur doped molybdenum in MoS<sub>2</sub> drops by about 1%, 1.5%, 4%, 8%, 11%, 15%, and 19% in comparison to the pristine MoS<sub>2</sub>. Increasing the percentage of sulfur doping in the MoS<sub>2</sub> sheet, the elastic properties decrease. Further, we found that the elastic properties due to sulfur vacancy defects with different percentages drop in great detail when compared the elastic properties due to diffusion at the respective percentage as deduce from Tables 2 and 3.



**Figure 5.** The atomistic model of monolayer MoS<sub>2</sub> with different percentage of antisite defects.

Figure 6 shows the effect of antisite defects molybdenum diffusion in sulfur, also dwindle the elastic constants of MoS<sub>2</sub> for the different defect fractions. The change of fractions were in ranges from 0.1% to 25% antisite defects. We started to pile-up the antisite defects and observed the elastic constants becomes more efficient and started to hinder further with the increase in the diffusion, unlike in case of pure defects where we seen the elastic properties drop dramatically with each defect fraction. The elastic constants  $C_{ij}$  of antisite defect also shows the trend of decrease in nature when compared to defect-free structure, it decreases from 139.69 N/m for 5% defects to 113.83 N/m for 25 % defects when compared to the of pure defects as seen in Table 3. In order to provide the results of impact of the antisite defect in MoS<sub>2</sub> sheet, again we prepared the random antisite defect models. Hundreds of replications were considered for MoS<sub>2</sub> with 0% to 25% antisite defects.



**Figure 6.** The elastic constants of MoS<sub>2</sub> as a function antisite defect fraction: (a)  $C_{11}$ , (b)  $C_{22}$ , (c)  $C_{12}$ .

#### 4. Conclusions

The elastic constants for MoS<sub>2</sub> monolayer using molecular statics simulation in great detail were investigated. MoS<sub>2</sub> is flexible and isotropic for small deformations and the results obtained from this study are compared with the previous literature for defect-free MoS<sub>2</sub> and progress towards higher defect fractions. The random distribution of defects in the MoS<sub>2</sub> sheet in addition to antisite defects were also discussed in great detail.

We have seen that the elastic constants of MoS<sub>2</sub> started dwindling at a rapid rate with the defects pile-up. It started to dwindle at a slow rate of up to 1% of defects. Just as the defects increase to 2% and beyond, its reduction began dramatically. Hence, when the defect percentage reaches 10%, the reduction in elastic constants was as huge as 28.8%. These vacancy defects greatly influenced the elastic behavior of the MoS<sub>2</sub> lattice. With the increase in defects fraction, the vector sum of displacement

affected the geometrical symmetry of the MoS<sub>2</sub> sheet. Moreover, in this study, we reviewed the possibility of physical properties improvement, and strengthening the elastic stiffness properties due to defects in MoS<sub>2</sub> was confirmed.

We also study the elastic constants for Mo as antisite defects, molybdenum diffusion in sulfur layers in the MoS<sub>2</sub> nanosheet for different defect concentrations ratios ranging from (0.1% to 25%) by using molecular statics simulation. We confirmed that Mo diffusion as the antisite defects indeed decreases the elastic constants in the MoS<sub>2</sub> nanosheet. Nevertheless, with the increase in defect concentration, Mo diffusion has also shown the decrease in tendency of elastic properties. Mainly, when the antisite defects concentration at 5% to 25%, we see the elastic stiffness decreases less than in comparison to pure defect structures.

**Author Contributions:** Conceptualization, W.K., M.J.A. and T.B.; methodology, M.J.A., W.K. and T.B.; software, M.J.A. and A.M.; validation, M.J.A. and W.K.; formal analysis, M.J.A.; investigation, M.J.A. and W.K.; resources, W.K.; data curation, M.J.A.; writing—original draft preparation, M.J.A.; writing—review and editing, W.K. and T.B.; visualization, M.J.A.; supervision, W.K.; project administration, T.B.; funding acquisition, T.B., W.K. and A.M. All authors have read and agreed to the published version of the manuscript.

**Funding:** The research is funded within the National Science Centre, Poland, project no. 2016/21/B/ST8/02450.

**Acknowledgments:** Calculations were performed in part at the Interdisciplinary Centre for Mathematical and Computational Modelling at the University of Warsaw under grant GB80-16.

**Conflicts of Interest:** The authors declare no conflict of interest

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